Comparitive Structural Analysis of High Rise Buildings with different Geometrical Plan using Floor Diaphragm

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Abstract— In this study, comparative structural analyses of three-dimensional (3-D) G+20 high-rise buildings with and without rigid floor diaphragm have been considered. The three different building plans hexagonal, pentagonal and square are considered. The buildings are also considered with different elevation floors that are 5 floors, 10 floors, 15 floors and 20 floors. The building are analyzed for four different Indian seismic zones (zone II, III, IV and V) as per IS 1893-2002. Total 96 buildings are analyzed with 27 load combinations. The buildings are critically analyzed to quantify the effects of various parameters for maximum axial forces, bending moment and shear force in beams, seismic forces, wind forces and floor displacements. The results show that using rigid diaphragm is more efficient in reducing above parameters in buildings for lateral forces. Rigid diaphragm concept is reasonable for building square in plan rather than pentagonal or hexagonal building plan.

Index Terms— Bending moment, Displacement; Rigid floor diaphragm, Seismic loading.

1 INTRODUCTION

To overcome the scarcity of space in the urban areas, high-rise build- Kim et al. (2003) modelled the building structures without the floor ings are the hallmark of modern society. The need for high-rise build- slabs assuming that they would have negligible effects on the response ings is increasing in our country day by day as land is becoming of a structure. The floor slabs are simply replaced by rigid floor diascarce which is encouraging the commercial utilization and the con- phragms for the efficiency in the analysis. Beams and floor slabs are struction of high-rise buildings. Behaviour of high-rise buildings to divided into several elements thus more time is required for the analyseismic lateral forces has to be critically examined considering vari- sis procedure and resolved the problems, efficient analytical modelous geometrical, parameters. Most commonly used horizontal struc- ling methods employing the sub structuring techniques, supertural systems for strengthening buildings against lateral force are dia- elements, and rigid diaphragms were adapted. The analytical results of phragm and trussing system. Diaphragm is a building component that time history analysis and the computational time of various analyses transmits lateral force to vertical force resisting components. Some of for example structures were compared to investigate the validity of the the prominent research works carried out on the floor diaphragm is as proposed modelling techniques proposed.

follows: Basu and Jain (2004) studied the center of rigidity for rigid floor dia-Moon and Lee (1994) proposed efficient model for high-rise structure phragm buildings that has been extended to unsymmetrical buildings including inplane floor slab flexibility without reducing the accuracy with flexible floors. They proposed a procedure ensures that the resulof the analysis, and also proposed a floor flexibility index whose im- tant member force is close to that of rigid floor buildings as the floor pacts are researched through parametric studies in terms of seismic diaphragm rigidity increases. A superposition-based methodology was base shear and its distribution, and displacement at the roof. The result proposed to execute code-specified torsional provisions for structures shows that it is desirable to include the inplane deformation of floor with flexible floor diaphragms. The result showed that resultant memslabs in the earthquake analysis of structures for economical and safe ber force is close to that of rigid floor diaphragm buildings as the floor design when the inplane deformation of floor slabs is expected to be diaphragm rigidity increases and also it was seen that treating the dialarge. phragms of structures as rigid for torsional analysis may cause consid-

erable error. comparison of results in terms of minimum and maximum moments, Bull et al. (2008) explored the trends and magnitude of forces in con- axial forces, shear forces in columns and beams, seismic forces and crete floor diaphragms for seismic loading. A new pseudo-Equivalent displacements are carried out. Following steps are adopted in the pre-Static Analysis (pESA) method for determining inertial forces in floor sent study:-

diaphragms was analyzed. Step-1 Selection of building geometries and story (3 geometry plan Hadianfard and Sedaghat (2013) studied the non-linear response of and G+20 storevs)

flexible concrete floor diaphragm with braced steel building under Step-2 Selection of diaphragm models – with and without rigid floor both dynamic ground motions and static lateral loads. The results were (2 types)

compared with rigid diaphragms. The study explained that span ratio Step-3 Selection of four seismic zones (II, III, IV, V)

was important parameter in flexibility of floor diaphragm. The results Step-4 Formation of load combination (27 load combinations)

showed that the maximum drift and displacement of flexible floor Step-5 Modelling of building using STADD.Pro software

diaphragm was higher than in rigid floor diaphragm. Yield base shears Step-6 Comparison of results in terms of minimum and maximum and initial stiffness of flexible floor diaphragm were higher than for bending moment, axial forces, and shear forces in columns and rigid diaphragm. For span ratio greater than 3:1 in low rise buildings beams, seismic forces and displacement.

the ultimate base shear capacities reduces significantly in flexible STRUCTURAL MODELLING AND ANALYSIS

floor diaphragm rather than in case of the rigid floor diaphragm analy- (a) Modelling of building frames

sis. Building frame with the following three geometrical configurations in Rehan and Mahure (2014) discussed the design and analysis of G+15 plan as shown in Fig. 1 are considered for analysis-

stories R.C.C., steel and composite building under effect of earth-CASE-1: Square building frame 15 m \times 15 m in plan area and 20 quake and wind using STAAD Pro. The result showed that steel-storey height.

concrete composite building performed better. CASE-2: Pentagonal building frame inscribed in $15 \text{ m} \times 15 \text{ m}$ plan Shivare et al. (2014) carried out earthquake analysis of high- rise area and 20 storey height.

buildings considering four buildings of same area but different geo-CASE-3: Hexagonal building frame inscribed in 15 m \times 15 m plan metrical plan. The result showed that diaphragm modelling has major area and 20 storey height.

influence on moment and displacement. Building frame with different elevations are considered for analysis The objective of the present study is (i) to compare the structural for all the above mentioned plans as follows:

analyses of three-dimensional (3-D) G+20 high-rise buildings with TYPE 1: Regular building frame.

and without floor diaphragm, (ii) to perform the analysis on three TYPE 2: Regular building frame having section cut from 5th floor to building plans, viz. hexagonal, pentagonal and square. The buildings 20th floor.

are also considered with different elevation floors that are 5 floors, 10 TYPE 3: Regular building frame having section cut from 10th floor to floors, 15 floors and 20 floors, (iii) to carry out the analyzed for four 20th floor.

different Indian seismic zones (zone II, III, IV and V) as per IS 1893- TYPE 4: Regular Building Fame having section cut from 15th floor to 2002. Total 96 buildings are analyzed with 27 load combinations, and 20th floor.

(iv) to quantify the effects of various parameters minimum and maxi- The Fig. 2 shows the different elevation for square plan building and mum bending moment, axial forces, and shear forces in columns and similar elevations are for the pentagonal and hexagonal plan buildbeams, seismic forces and floor displacement on buildings with and ings.

without rigid floor diaphragm.

Number of beams and columns for these cases are given in Table 1.

(b) Types of diaphragm

2. METHODOLOGY

The following two types of diaphragm conditions have been consid-

A comparative study of G +20 high- rise building for different geo- ered for analysismetrical plans and diaphragm constraints under seismic loading. A Type-A: Model without rigid floor diaphragm constraint.

Type-B: Model with rigid floor diaphragm constraint ing moment in beams decrease in series from pentagonal, hexago-(c) Material and geometrical properties nal to square building plan. It can be observed that bending mo-Material properties have been considered in the modelling are density ments can be drastically reduced using rigid floor diaphragm by of RCC: 25 kN/m3, density of masonry: 20 kN/ m3 Young's modulus about 40 - 50%. of concrete: 2.17185 × 1016 N/m2, Poisson ratio: 0.17 b. Axial force The foundation depth is considered at 3.5m below ground level and Minimum and maximum axial force in columns is shown in the typical storey height is 3.5 m. The column size is $450 \text{ mm} \times 450$ Figs. 5 and 6 and Tables 5 and 6, respectively. The minimum mm, and the beam size is $350 \text{ mm} \times 500 \text{ mm}$. axial force in column are observed in building frame having (d) Loading conditions square plan with floor diaphragm and maximum axial force in Following loading are conducted for analysis column are observed in building frame having pentagonal plan Dead loads: as per IS 875-1987 (Part 1) without floor diaphragm. The axial force in columns has are not Self weight of slab for 150 mm thick. slab = $0.15 \times 25 = 3.75$ kN/m2 so much affected by using floor diaphragm. Floor finish load = 1 kN/ m2c. Shear force Water proofing load on roof = 2.5 kN/m2Minimum and maximum shear force in beam is shown in Figs. Masonry wall load = $0.20 \times 2.55 \times 20 = 10.2$ kN/m 7 and 8 and Tables 7 and 8, respectively. The minimum shear Live loads: on typical floors = 2 kN/ m2 as per IS 875-1987 (Part 2) Seismic load: All the building frames are analyzed for four seismic force in beam is observed in building frame having square plan zones. The seismic load are derived for following seismic parameters with floor diaphragm. Maximum shear force in beam is obas per IS: 1893-2002 (part 1) served in building frame having hexagonal plan without floor a. Seismic zones: II, III, IV, V diaphragm. Maximum shear force in beams is lesser in building b. Response reduction factor (R): 5 frame with floor diaphragm. And it has been reduced by about c. Importance factor (I): 1 45 - 55%. d. Damping: 5% d. Displacement e. Soil type: medium soil Maximum displacement in X- and Z- transmissions are shown (e) Structural Analysis Structural analyses of the building frames are carried out using in Figs. 9 and 10 and Tables 9 and 10, respectively. Maximum

STAAD.Pro software. All the columns are rigidly supported at ground displacement is observed in building frame having pentagonal and 27 load combinations, given in Table 2, are considered for the plan without floor diaphragm. By application of floor diaanalysis purposes. Application of boundary and loading conditions are phragm the displacement is reduced by about 35 - 45 % done through the GUI mode of the software.

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3. RESULTS AND DISCUSSION

The results of seismic analyses of G+20 building with and without rigid floor diapgragm are as follows:

a. Bending moments

The minimum and maximum bending moments in beams for different cases are shown in Figs. 3 and 4 and Tables 3 and 4, respectively. The minimum bending moment in beams are oserved in building frame having square plan with floor diaphragm and the maximum bending moment in beams are observed in building frame having pentagonal plan without floor diaphragm. The bend426

Table 1: Number of beams and columns in different cases

| | er | Square | Pentago | onal | He | xagonal | Table 4 Manimum han die | | · | |
|---------------------------------------|----------------------------------------------|-----------------------------|--------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------|
| Columns 756 | | 273 | | 357 | , | | e 4 Maximum bending moments in beams | | | |
| Beams 1260 | | 420 58 | | 588 | | Comparison of maxi | mum bending | g moments in b | eams | |
| Table 2: Different load any bin time. | | | | | | | | Moment M_z in kNm | | |
| Table 2: Different load combinations | | | | | | | Case | [beam] (node number) | | |
| Load | EQ IN X DIR. | | | Load | | | | Square | Pentagonal | Hexagona |
| case | | | | | | e detail | | 325.290 | 428.524 | 392.495 |
| no. | | | | no. | | | | [144] (39) | [34] (1) | [271] (103 |
| 1. | | | | 14. | 0.9 DL + 1.5 EQX | | Floor diaphragm | Type 2 | Type 1 | Type 2 |
| 2. | EQ IN 2 | | | 15. | 0.9 DL - 1.5 EQX | | - | Zone 5 | Zone 5 | Zone 5 |
| 3. | DEAD | | | 16. | 0.9 DL + 1.5 EQZ | | | 568.368 | 803.083 | 791.320 |
| 4. | LIVE LOAD 1.5 (DL + LL) 1.5 (DL + EQX) | | | 17. | 0.9 DL - 1.5 EQZ 1.0 (DL + LL) | | | [509] (326) | [230] (106) | [355](147 |
| 5. | | | | 18. | | | Without floor diaphragm | Type 3 | Type 1 | Type 2 |
| 6. | | | | 19. | 1.0 (DL + | - / | | Zone 5 | Zone 5 | Zone 5 |
| 7. | 1.5 (DL | - / | QX) 20. 1.0 | | 1.0 (DL - | | | | | |
| 8. | 1.5 (DL + EQZ) 21. 1.0 (DL + EQZ) | | | - EQZ) | Table 5 Minimum axial force in columns | | | | | |
| 9. | 1.5 (DL - EQZ) 22. 1.0 (DL - EQZ) | | EQZ) | Comparison of minimum axial force in columns | | | | | | |
| 10. | 1.2 (DL | 1.2 (DL + LL + EQX) 23. 0.8 | | 0.8 (DL + | - LL + EQX) | | Axial force F_x (kN) | | | |
| 11. | 1.2 (DL | (DL + LL - EQX) 24. 0. | | 0.8 (DL + | - LL - EQX) | Case | [column] (node number) | | | |
| 12. | 1.2 (DL | + LL + EQ | Z) 2 | 25. | 0.8 (DL + LL + EQZ) | | | Square | Pentagonal | Hexagona |
| 13. | 1.2 (DL | + LL - EQ2 | Z) [] | 26. | 0.8 (DL + | - LL - EQZ) | | 390.950 | 747.389 | 640.281 |
| | `` | | | | | | | | | |
| | , , | | | 27. | LOAD F | OR CHECK | Eleor dianhragm | [106] (6) | [22] (2) | [29] (1) |
| | | | | | | OR CHECK | Floor diaphragm | [106] (6) Type 3 | [22] (2) Type 3 | [29] (1) Type 2 |
| | 3 Minim | um bendi | ng mom | ents i | n beams | | Floor diaphragm | | | |
| | 3 Minim | | ng mom | ents i | | | Floor diaphragm | Type 3 | Type 3 | Type 2 |
| | 3 Minim | | ng mom | ents i | n beams | beams | | Type 3 Zone 2 | Type 3 Zone 2 | Type 2 Zone 2 |
| | 3 Minim | | ng mom | ents i nding 1 Mo | n beams moments in | beams kNm | Floor diaphragm Without floor diaphragm | Type 3 Zone 2 518.870 | Type 3 Zone 2 1008.540 | Type 2 Zone 2 836.990 |
| | 3 Minimu Compari | | ng mom | ents i nding i Mo [bea | n beams moments in ment M_z in m] (node nu | beams kNm | Without floor diaphragm | Type 3 Zone 2 518.870 [110] (5) | Type 3 Zone 2 1008.540 [21] (1) | Type 2 Zone 2 836.990 [29] (1) |
| | 3 Minimu Compari | | ng mom | nding r Mo [bea re | n beams moments in ment M_z in m] (node nu | beams kNm mber) | Without floor diaphragm | Type 3 Zone 2 518.870 [110] (5) Type 4 | Type 3 Zone 2 1008.540 [21] (1) Type 2 | Type 2 Zone 2 836.990 [29] (1) Type 2 |
| [able 3 | 3 Minimu Compari Case | ison of min | ng mom imum ber Squar | nding r Mo [bea re 11 | n beams moments in ment M_z in m] (node nu Pentagonal | beams kNm mber) Hexagonal | Without floor diaphragm | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 | Type 2 Zone 2 836.990 [29] (1) Type 2 |
| fable 3 | 3 Minimu Compari | ison of min | ng mom imum ber Squar 76.71 | nding r Mo [bea re 11 (1) | n beams moments in oment M_z in 7 m] (node nu Pentagonal 112.631 | beams kNm mber) Hexagonal 97.910 | Without floor diaphragm | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in colum | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mms | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 |
| [able 3 | 3 Minimu Compari Case | ison of min | ng mom imum ber Squar 76.71 [106] (| nding r Mo [bea re [1] (1) 2 4 | n beams moments in ment M_z in m] (node nu Pentagonal 112.631 [199] (81) | beams kNm mber) Hexagonal 97.910 [496] (188) | Without floor diaphragm Table 6 Maximum axial fo | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in columnation | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mms | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 |
| [able 3 | 3 Minimu Compari Case | ison of min | ng mom imum ber Squar 76.71 [106] (Type | ments i nding r [bear re 11 (1) 2 4 2 2 | n beams moments in ment M_z in 1 m] (node nu Pentagonal 112.631 [199] (81) Type 2 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 | Without floor diaphragm Table 6 Maximum axial fo | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in columnation aximum axial | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 uns |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone | nding r Mo [bear re 11 (1) 2 4 2 2 | n beams moments in ment M_z in m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 | Without floor diaphragm Table 6 Maximum axial for Comparison of m | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in columnation aximum axial | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns force in column xial force F_x in | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 uns kN mber) |
| Fable 3 | 3 Minimu Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 | eents i nding r [bea: re [1] (1) 2 4 2 2 7 303) | n beams moments in ment M_z in m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 | Without floor diaphragm Table 6 Maximum axial for Comparison of m | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in colu: aximum axial | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns force in colum xial force F_x in umn] (node nu Pentagonal | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 ms kN mber) Hexagor |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 [606] (3 | re [bear (1) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 | n beams moments in ment M_z in m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 [210] (92) | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 [376] (152) | Without floor diaphragm Table 6 Maximum axial fo Comparison of m Case | Type 3 Type 2 518.870 [110] (5) Type 4 Zone 2 orce in columnation aximum axial A [col Square 5467.306 | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns force in column xial force F_x in umn] (node nu Pentagonal 9108.521 | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 Ins kN mber) Hexagor 9815.01 |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 [606] (3 Type | re [bear (1) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 | n beams moments in ment M_z in main m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 [210] (92) Type 1 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 [376] (152) Type 1 | Without floor diaphragm Table 6 Maximum axial for Comparison of m | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in colu: aximum axial [col Square 5467.306 [111] (6) | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns force in column exial force F_x in umn] (node nu Pentagonal 9108.521 [26] (21) | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 NN kN mber) Hexagon 9815.01 [80] (19 |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 [606] (3 Type | re [bear (1) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 | n beams moments in ment M_z in main m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 [210] (92) Type 1 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 [376] (152) Type 1 | Without floor diaphragm Table 6 Maximum axial fo Comparison of m Case | Type 3 Type 2 518.870 [110] (5) Type 4 Zone 2 orce in columnation aximum axial A [col Square 5467.306 | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mms I force in column xial force F_x in umn] (node nu Pentagonal 9108.521 [26] (21) Type 1 | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 nns kN mber) Hexagor 9815.01 [80] (19 Type 1 |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 [606] (3 Type | re [bear (1) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 | n beams moments in ment M_z in main m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 [210] (92) Type 1 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 [376] (152) Type 1 | Without floor diaphragm Table 6 Maximum axial fo Comparison of m Case | Type 3 Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in column aximum axial A [col Square 5467.306 [111] (6) Type1&2 Zone 5 | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mns I force in column xial force F_x in umn] (node nu Pentagonal 9108.521 [26] (21) Type 1 Zone 5 | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 ns .kN mber) Hexagor 9815.01 [80] (19 Type 1 Zone 5 |
| Fable 3 | 3 Minima Compari Case | ragm | ng mom imum ber Squar 76.71 [106] (Type Zone 107 [606] (3 Type | re [bear (1) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 | n beams moments in ment M_z in main m] (node nu Pentagonal 112.631 [199] (81) Type 2 Zone 2 171.120 [210] (92) Type 1 | beams kNm mber) Hexagonal 97.910 [496] (188) Type 3 Zone 2 117.270 [376] (152) Type 1 | Without floor diaphragm Table 6 Maximum axial fo Comparison of m Case | Type 3 Zone 2 518.870 [110] (5) Type 4 Zone 2 orce in colum aximum axial Column Square 5467.306 [111] (6) Type1&2 | Type 3 Zone 2 1008.540 [21] (1) Type 2 Zone 2 mms I force in column xial force F_x in umn] (node nu Pentagonal 9108.521 [26] (21) Type 1 | Type 2 Zone 2 836.990 [29] (1) Type 2 Zone 2 ms kN mber) Hexagor |

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| Type1&2 | Type 1 | Type 1 | | 434.062 | 961.174 | 806.143 |
|---------|--------|--------|-------------------------|---------|---------|---------|
| Zone 5 | Zone 5 | Zone 5 | Without floor diaphrasm | (393) | (276) | (370) |
| | | | Without floor diaphragm | Type 3 | Type 2 | Type 2 |
| | | | | Zone 5 | Zone 5 | Zone 5 |

Table 7 Minimum shear force in beams

| Comparison of minimum shear force in beams | | | | Table 10 Maximum displacement in Z transmission | | | | |
|--------------------------------------------|---------------------------------------------|--------------|--------------|---------------------------------------------------|------------------------------------|------------|-----------|--|
| Case | Shear force F_y (kN) [beam] (node number) | | | Comparison of maximum displacements | | | | |
| Cuse | | - , | , | Case | Z-transmission in mm (node number) | | | |
| | Square | Pentagonal | Hexagonal | Case | Square | Pentagonal | Hexagonal | |
| | 43.480 | 111.900 | 121.828 | | 271.837 | 358.873 | 426.875 | |
| Eleon dianhram | [106] (1) | [86] (52) | [132] (68) | | (127) | (281) | (358) | |
| Floor diaphragm | Type 4 | Type 1,2,3&4 | Type 1,2,3&4 | Floor diaphragm | · · · | · | . , | |
| | Zone 2 | Zone 2 & 3 | Zone 2 & 3 | | Type 1 | Type 1 | Type 1 | |
| | 104.630 | 142.097 | 153.273 | | Zone 5 | Zone 5 | Zone 5 | |
| | | | | Without floor diaphragm | 423.358 | 738.271 | 698.182 | |
| Without floor diaphragm | [496] (308) | [332] (134) | [400] (164) | | (132) | (276) | (362) | |
| 1 0 | Type 1 | Type 3 | Type 1 | | Type 3 | Type 1 | Type 1 | |
| | Zone 2 | Zone 2 | Zone 2 | | Zone 5 | Zone 5 | Zone 5 | |
| | | | | J | Zone 5 | Zone 5 | Zone 5 | |

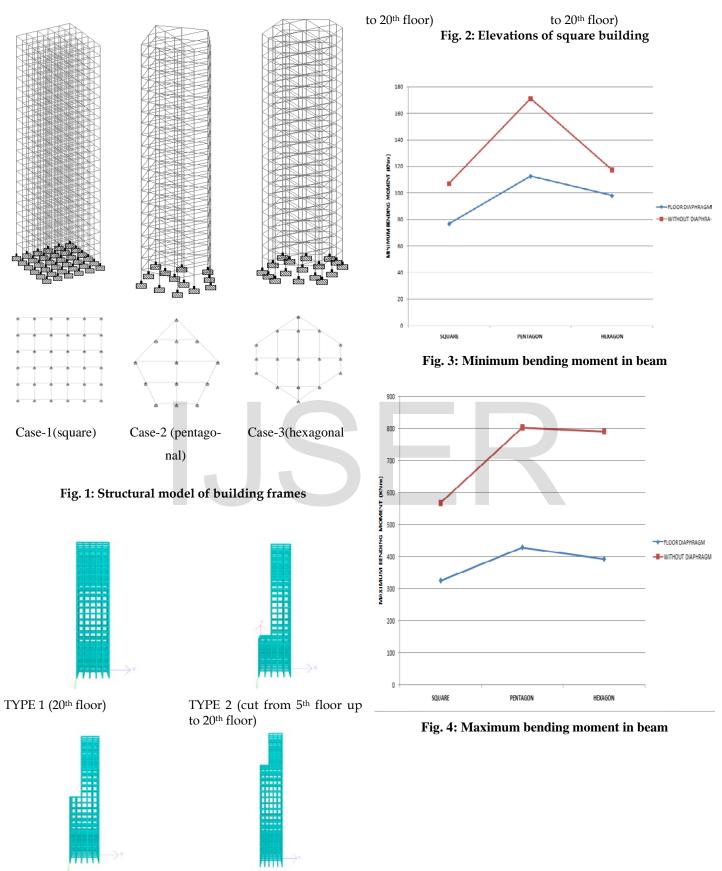
Table 8 Maximum shear force in beams

| Comparison of maximum shear force in beams | | | | | |
|--------------------------------------------|-------------------------------------------------|-------------|-----------|--|--|
| Case | Shear force F_y in kN [beam] (node number) | | | | |
| | Square | Pentagonal | Hexagonal | | |
| | 180.517 | 237.754 | 217.956 | | |
| Floor diaphragm | [144] (39) | [21] (1) | [29] (1) | | |
| ribbi diapinagin | Type 3 | Type 1 | Type 1 | | |
| | Zone 5 | Zone 5 | Zone 5 | | |
| | 402.984 | 444.671 | 473.378 | | |
| Without floor diaphragm | [509] (326) | [230] (106) | [68] (39) | | |
| | Type 3 | Type 1 | Type 4 | | |
| | Zone 5 | Zone 5 | Zone 5 | | |

Table 9 Maximum displacement in X transmission

| Comparison of maximum displacements | | | | | | |
|-------------------------------------|------------------------------------|------------|-----------|--|--|--|
| Case | X-transmission in mm (node number) | | | | | |
| Cuse | Square | Pentagonal | Hexagonal | | | |
| | 345.456 | 516.427 | 435.739 | | | |
| Floor diaphragm | (129) | (276) | (358) | | | |
| ribbi diapinagin | Type 2 | Type 2 | Type 2 | | | |
| | Zone 5 | Zone 5 | Zone 5 | | | |

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TYPE 3 (cut from 10th floor up TYPE 4 (cut from 15th floor up

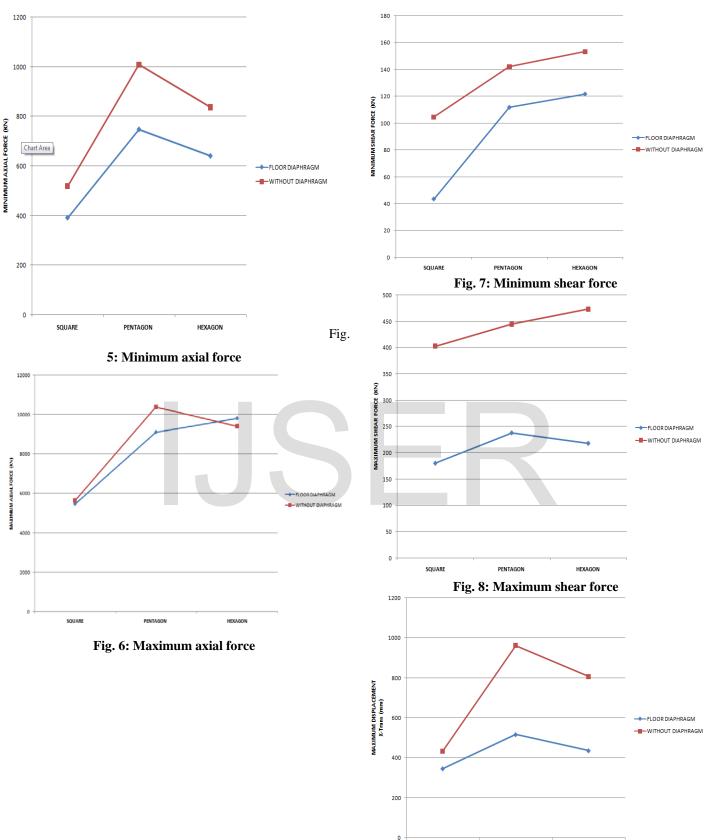


Fig. 9: Maximum displacement in X transmission

HEXAGON

PENTAGON

SQUARE

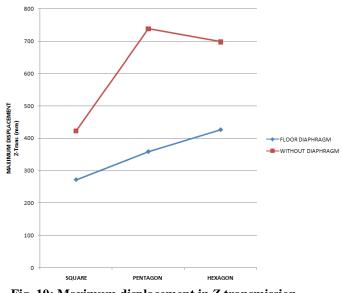


Fig. 10: Maximum displacement in Z transmission

4 CONCLUSION

In this study, a comparative structural analysis of 3-D G+20 high-rise buildings with and without rigid floor diaphragm is 11. carried out. The results of this parametric study shows that rigid floor diaphragm modelling has major influence on bending moment, axial force, shear force and displacement of the high-rise buildings. The analyses show that the rigid floor diaphragm is more effective in reducing seismic responses in square buildings.

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